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Dynamic Aeroelastic Scaling of the CRM Wing via Multidisciplinary Optimization

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WCSMO12



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Introduction - Similarity and Optimization



Reference aircraft

Introduction - Similarity and Optimization



Reference aircraft

Scaled model



- Thicknesses → Passive action on [K] & [M]
- Moving Masses → Active action on [M]
- PZT → Active action on [K]

Introduction - Similarity and Optimization



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Introduction - Similarity and Optimization



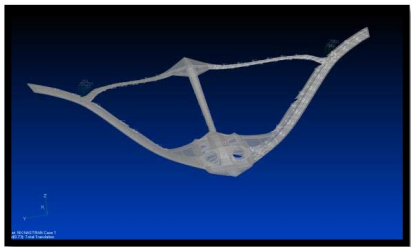
Reference aircraft

Scaled model

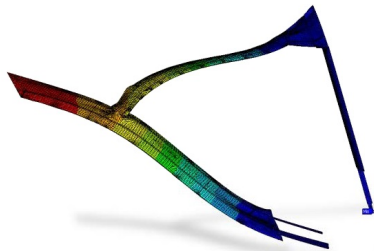


- Thicknesses → Passive action on [K] & [M]
- Moving Masses → Active action on [M]
- PZT → Active action on [K]

Introduction - Dynamic Aeroelastic Similarity



Reference aircraft mode shape*



Optimized scale demonstrator mode shape*



*[Richards et al., AIAA/ATIO Conference, 2010]

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- 4 Aerodynamic Flutter Optimization
- 5 Conclusion
- 6 Perspectives

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- Nastran 95*: Normal Modes and Flutter Analysis

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- Panair/a502†: Static aerodynamics

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- OpenMDAO‡ Framework



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- Optimizer: SLSQP (Gradient-based, from Scipy library)



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 *[\[github.com/nasa/NASTRAN-95\]](https://github.com/nasa/NASTRAN-95)

 †[\[pdas.com/panair.html\]](http://pdas.com/panair.html)

 ‡[\[Gray et al., AIAA/ISSMO, 2014\]](#)

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Dynamic Aeroelastic Scaling

Aeroelastic equations of motion:

$$[\mathbf{M}]\{\ddot{x}\} + [\mathbf{K}]\{x\} = [\mathbf{A}_k]\{x\} + [\mathbf{A}_c]\{\dot{x}\} + [\mathbf{A}_m]\{\ddot{x}\} + [\mathbf{M}]\{a_g\}$$

Dynamic Aeroelastic Scaling

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In modal coordinates ($\{x\}=[\Phi]\{\eta\}$):

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$$[\Phi]^T[\mathbf{M}][\Phi]\{\ddot{\eta}\} + [\Phi]^T[\mathbf{K}][\Phi]\{\eta\} = [\Phi]^T[\mathbf{A}_k][\Phi]\{\eta\} + \\ [\Phi]^T[\mathbf{A}_c][\Phi]\{\dot{\eta}\} + [\Phi]^T[\mathbf{A}_m][\Phi]\{\ddot{\eta}\} + \frac{1}{b}[\Phi]^T[\mathbf{M}]\{a_g\}$$

Dynamic Aeroelastic Scaling

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[Ricciardi et al., Journal of Aircraft, 2014]

Adimensionalize with reference quantities:

$$\begin{aligned}
 \langle \bar{\mathbf{m}} \rangle \{ \bar{\eta}^{**} \} + \langle \bar{\mathbf{m}} \bar{\omega}^2 \rangle \{ \eta \} &= \underbrace{\frac{V^2}{b^2 \omega_1^2}}_{1/\kappa_1^2} \underbrace{\frac{gb}{V^2}}_{1/Fr^2} \langle \bar{\mathbf{m}} \rangle [\Phi]^{-1} \{ \bar{a}_g \} \\
 + \underbrace{\frac{1}{2} \frac{\rho S b}{m_1}}_{\mu_1} \underbrace{\frac{V^2}{\omega_1^2 b^2}}_{1/\kappa_1^2} &\left([\bar{\mathbf{a}}_k] \{ \eta \} + \underbrace{\frac{\omega_1 b}{V}}_{\kappa_1} [\bar{\mathbf{a}}_c] \{ \bar{\eta}^* \} + \underbrace{\frac{\omega_1^2 b^2}{V^2}}_{\kappa_1^2} [\bar{\mathbf{a}}_m] \{ \bar{\eta}^{**} \} \right)
 \end{aligned}$$

Traditional Dynamic Aeroelastic Scaling

Nondimensional aeroelastic equations of motion (harmonic solution):

Reference aircraft: r

Scaled model: m

$$\langle \bar{\mathbf{m}}_r \rangle \{ \ddot{\eta}^* \} + \langle \bar{\mathbf{m}}_r \bar{\omega}_r^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} [\bar{\mathbf{a}}_{hr}(X_{ar}, \kappa, M_r)] \{ \eta \}$$

$$\langle \bar{\mathbf{m}}_m \rangle \{ \ddot{\eta}^* \} + \langle \bar{\mathbf{m}}_m \bar{\omega}_m^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} [\bar{\mathbf{a}}_{hm}(X_{am}, \kappa, M_m)] \{ \eta \}$$

Traditional Dynamic Aeroelastic Scaling

Nondimensional aeroelastic equations of motion (harmonic solution):

Reference aircraft: \mathbf{r}

Scaled model: \mathbf{m}

$$\underbrace{\langle \bar{\mathbf{m}}_{\mathbf{r}} \rangle \{ \bar{\eta}^{**} \} + \langle \bar{\mathbf{m}}_{\mathbf{r}} \bar{\omega}_{\mathbf{r}}^2 \rangle \{ \eta \}} = \frac{1}{2} \frac{\mu_{1\mathbf{r}}}{\kappa_{1\mathbf{r}}^2} \underbrace{[\bar{\mathbf{a}}_{\mathbf{hr}}(X_{\mathbf{ar}}, \kappa, M_{\mathbf{r}})] \{ \eta \}}$$

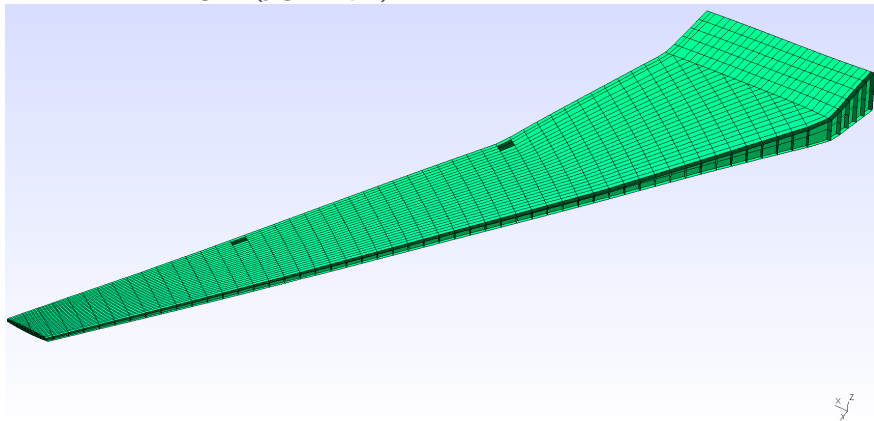
Match $[\Phi], \langle \bar{\omega} \rangle, \langle \bar{\mathbf{m}} \rangle$
(from the problem
 $K - \omega^2[\mathbf{M}]\{\phi\} = 0$)
through optimization

Equal if same aerodynamic
shape and flow similarity

$$\underbrace{\langle \bar{\mathbf{m}}_{\mathbf{m}} \rangle \{ \bar{\eta}^{**} \} + \langle \bar{\mathbf{m}}_{\mathbf{m}} \bar{\omega}_{\mathbf{m}}^2 \rangle \{ \eta \}} = \frac{1}{2} \frac{\mu_{1\mathbf{m}}}{\kappa_{1\mathbf{m}}^2} \underbrace{[\bar{\mathbf{a}}_{\mathbf{hm}}(X_{\mathbf{am}}, \kappa, M_{\mathbf{m}})] \{ \eta \}}$$

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Reference Design* (jig shape): For all elements $t_r = 8.89mm$



Model provided by T. Achard and C. Blondeau*

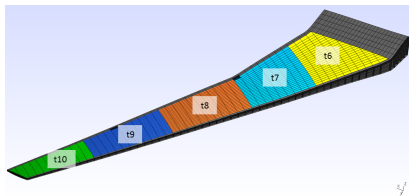


*[Achard et al., AIAA/ISSMO, 2016]

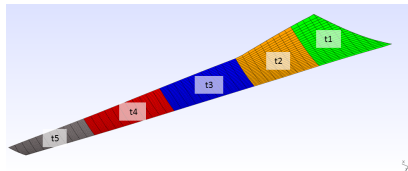
CRM modal optimization: Problem definition

Hypothesis: Flow similarity assumed

Objective Function		Dimension	Bounds
Mode shape difference minimization		$\min(N - \text{trace}(\text{MAC}([\Phi_r], [\Phi_m])))$	\mathbb{R}
Design Variables			
Skin thicknesses vector		$[t]$	\mathbb{R}^{10} [0.0889, 26.67] mm
Constraints			
Reduced frequency matching	$\ \omega_r - \omega_m\ = 0$	\mathbb{R}	
Mass matching	$M_r - M_m = 0$	\mathbb{R}	
Generalized masses matching	$\ m_r - m_m\ = 0$	\mathbb{R}	



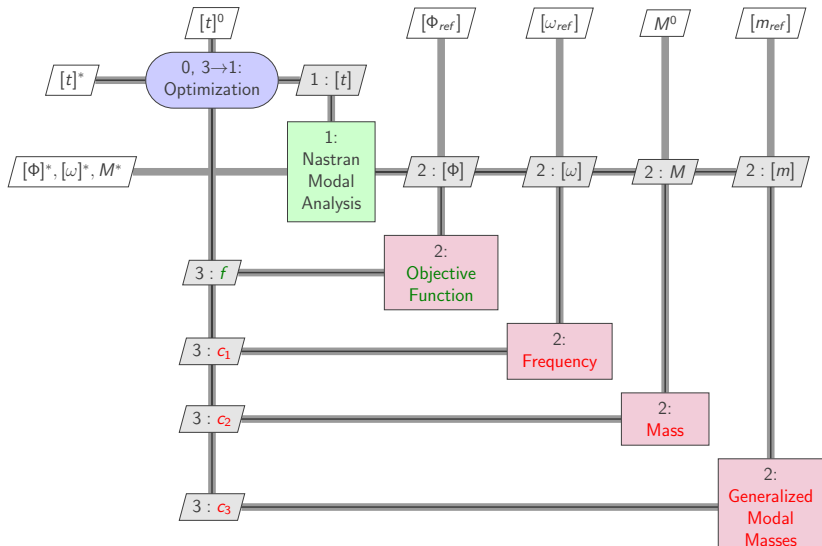
→ Upper skin panels



Lower skin panels ←

Traditional Modal Optimization

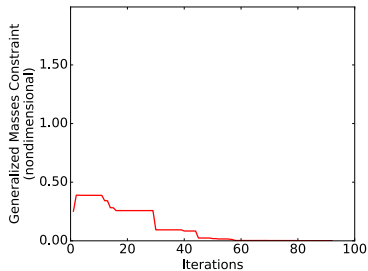
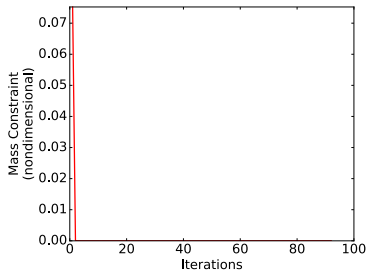
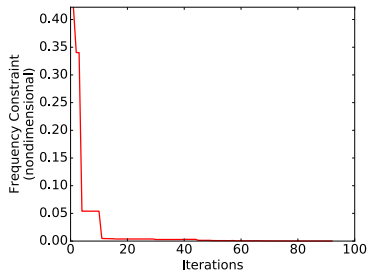
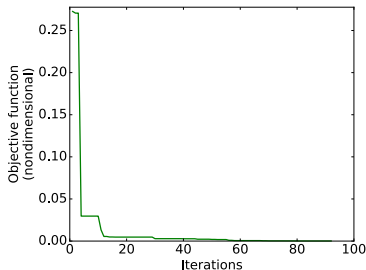
Hypothesis: Flow similarity assumed



CRM Modal Optimization: Results

Best Found Point vs Iteration

Criterion: Point with best objective function AND sum of constraints



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What if the flow is not similar?

Reference aircraft: r

Scaled model: m

$$\langle \bar{\mathbf{m}}_r \rangle \{ \bar{\eta}^{**} \} + \langle \bar{\mathbf{m}}_r \bar{\omega}_r^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} [\bar{\mathbf{a}}_{hr}(X_{ar}, \kappa, M_r)] \{ \eta \}$$

$$\langle \bar{\mathbf{m}}_m \rangle \{ \bar{\eta}^{**} \} + \langle \bar{\mathbf{m}}_m \bar{\omega}_m^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} [\bar{\mathbf{a}}_{hm}(X_{am}, \kappa, M_m)] \{ \eta \}$$

What if the flow is not similar?

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$$\underbrace{\langle \bar{\mathbf{m}}_r \rangle \{ \tilde{\eta}^{**} \} + \langle \bar{\mathbf{m}}_r \bar{\omega}_r^2 \rangle \{ \eta \}} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} \underbrace{[\bar{\mathbf{a}}_{hr}(X_{ar}, \kappa, M_r)]}_{\text{?}} \{ \eta \}$$

matched through modal optimization

$$\underbrace{\langle \bar{\mathbf{m}}_m \rangle \{ \tilde{\eta}^{**} \} + \langle \bar{\mathbf{m}}_m \bar{\omega}_m^2 \rangle}_{\text{?}} \{ \eta \} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} \underbrace{[\bar{\mathbf{a}}_{hm}(X_{am}, \kappa, M_m)]}_{\text{?}} \{ \eta \}$$

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What if the flow is not similar? Aerodynamic Optimization

- Reference aircraft: r
- Scale model: m

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- Reference aircraft: r
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- Reduced frequency: κ
- Mach number: M

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Objective function:

What if the flow is not similar? Aerodynamic Optimization

- Reference aircraft: \mathbf{r}
- Scale model: \mathbf{m}
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- Mach number: M

Objective function:

$$f = \sum_i (||[\bar{\mathbf{a}}_{\mathbf{hr}}(\mathbf{X}_{\mathbf{ar}}, \kappa_{\mathbf{i}}, M_{\mathbf{r}})] - [\bar{\mathbf{a}}_{\mathbf{hm}}(\mathbf{X}_{\mathbf{am}}, \kappa_{\mathbf{i}}, M_{\mathbf{m}})]||)$$

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Design variables:

What if the flow is not similar? Aerodynamic Optimization

- Reference aircraft: r
- Scale model: m
- Reduced frequency: κ
- Mach number: M

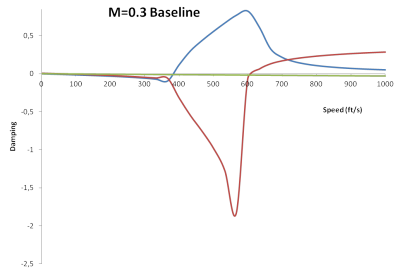
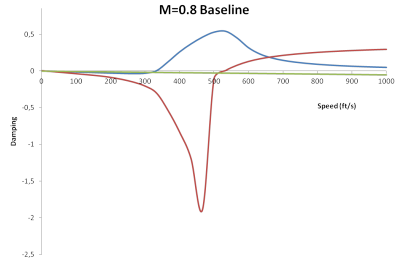
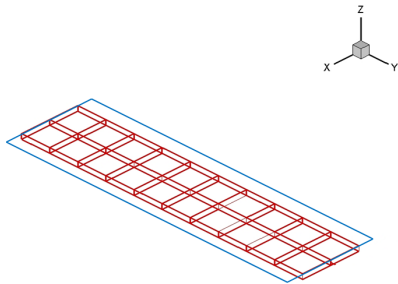
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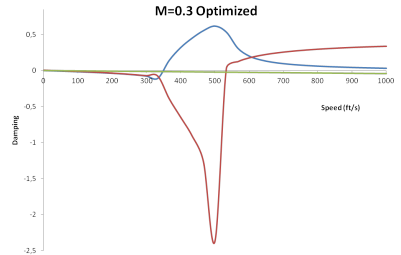
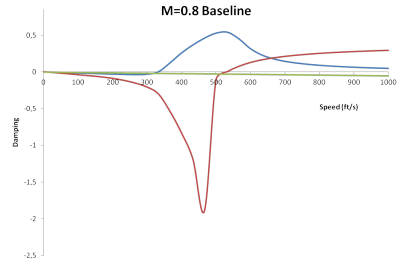
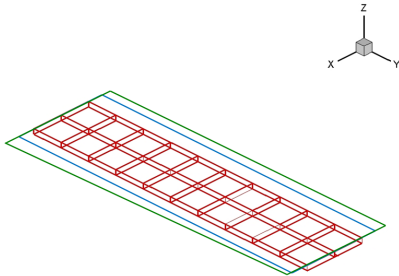
Design variables:

- X_{am} : Parameters defining the wing planform

Aerodynamic Optimization: Goland Wing Test Case



Aerodynamic Optimization: Golland Wing Test Case



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- Review of the traditional dynamic aeroelastic scaling approach

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- Modal optimization for similarity

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- Application to the CRM test case

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- Wing planform optimization for flutter similarity

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- Perform flutter-based wing planform optimization with the CRM model

- Perform flutter-based wing planform optimization with the CRM model
- From the optimized planform, optimize wing twist distribution and structure properties to match static deflection

This work has been supported by the EU project 658570 - NextGen Airliners funded by Marie Skłodowska-Curie actions (MSCA).

Thanks for your attention!

Questions?