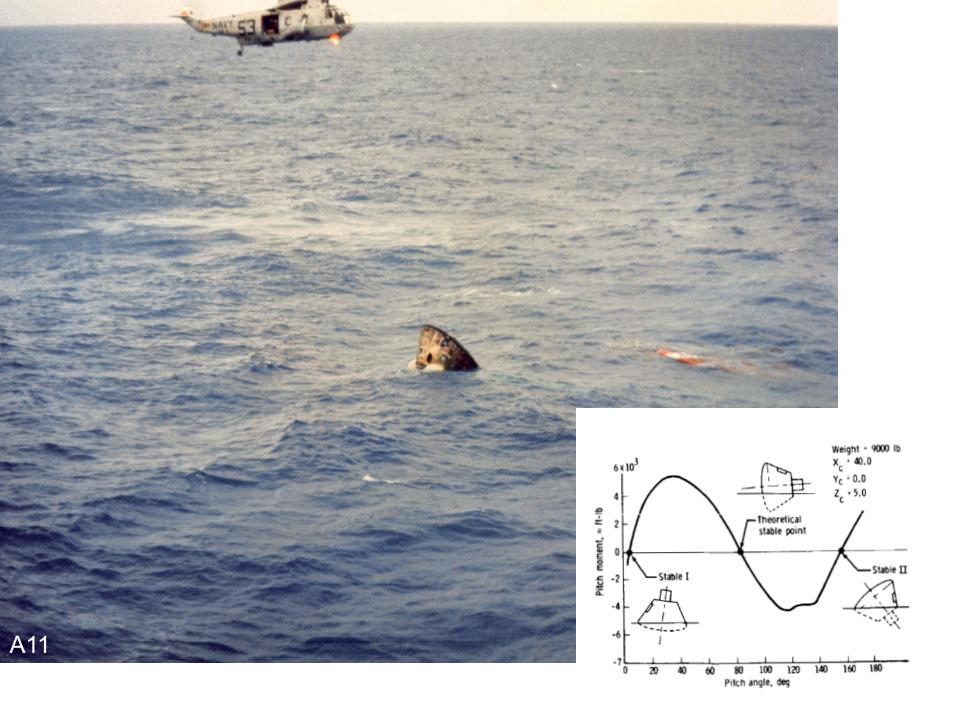


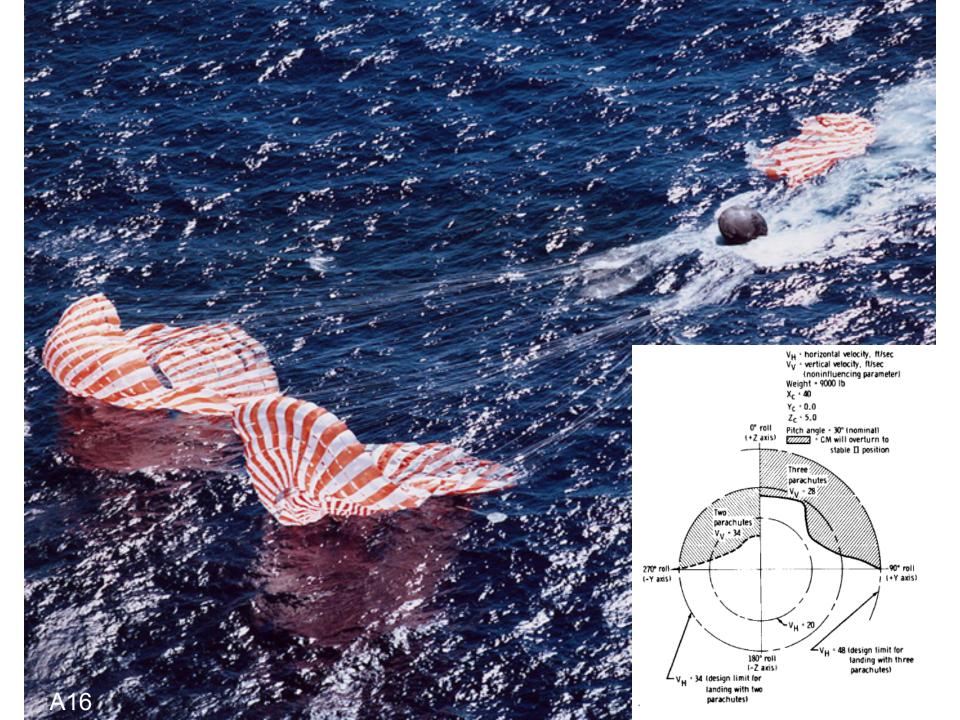
Ralph D Lorenz

JHU Applied Physics Laboratory, Laurel,, MD, USA

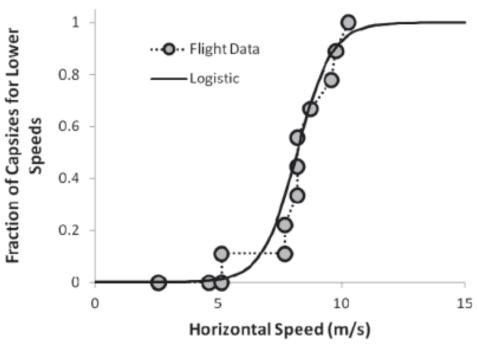
With thanks to Space Historian Daviid Harland, and filmmaker Stephen Slater







				Time	
	Wind	Waves		(mins) to	Weather from transcripts (Forecast unless otherwise noted) or from
	(m/s)	(m)	Capsize?	Stable I	mission reports (Skylab, ASTP)
AS 201	5.1	0.3			recovery photo estimate
AS 202	7.7	0.6			recovery photo estimate
Apollo 4	7.7	1.2			Two reports 15kts, 4ft waves w/ 8ft swell. One report 17-25kts, 8ft waves
Apollo 6	10.3	1.8	Υ	1	
Apollo 7	8.2	0.9	Y	12	
Apollo 8	9.8	1.8	Υ	6	12 kts, waves 4ft (after says 19kts, 6ft swell)
Apollo 9	4.6	2.2			Light/variable, 2-3 ft
Apollo 10	2.6	0.9			12kts, waves 5ft
Apollo 11	8.2	0.9	Y	7.6	18kts, waves 3-6ft
Apollo 12	7.7	0.9	Y	4.5	15kts, 3ft waves w/ 6ft swell (Ortloff/Harland says 15ft swell)
Apollo 13	5.1	1.2			10kts, waves 4ft
Apollo 14	7.7	1.2			15kts, 2ft waves@2s period with 4ft waves@3s
Apollo 15	5.1	0.9			18kts, waves approaching 6ft. Then 15kts, 4ft. One chute failed
Apollo 16	5.1	1.2	Y	4.5	10kts, 3ft waves
Apollo 17	5.1	0.6			10kts, 3ft waves
Skylab	2.6	0.3			0.3m waves on 1.2m swell. 2.6m/s
Skylab	9.6	0.5	Υ	5	0.5m waves. Wind 35 km/h
Skylab	8.2	0.6	Y	5	0.6m waves 2s period on 0.9m swell. 8.2 m/s
ASTP	8.7	1.1	Υ	4.5	17kts. 1.1m waves

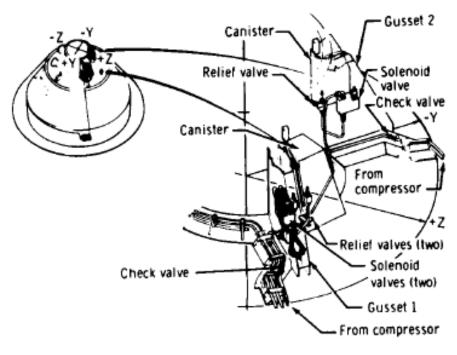


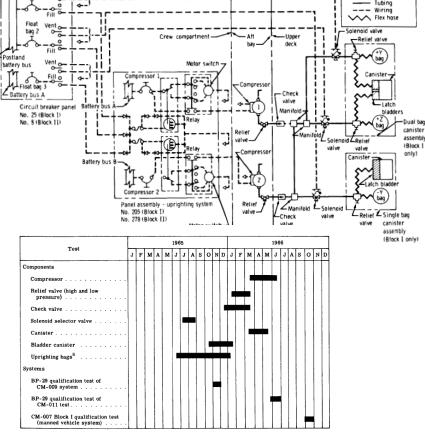
APOLLO EXPERIENCE REPORT - COMMAND MODULE UPRIGHTING SYSTEM

by Robert D. White Manned Spacecraft Center Houston, Texas 77058



NASA TN D-7081

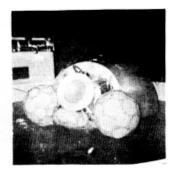


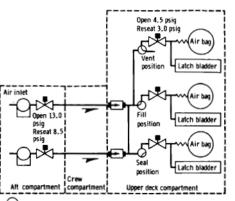














Air compressor, dc motor driven

Relie Chec

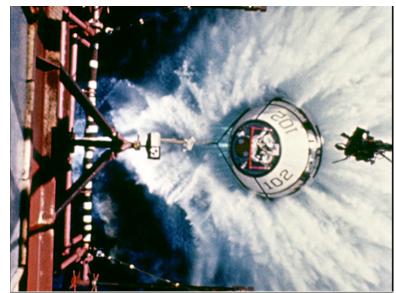
Check valve
Solenoid-operated valve, three port, three position

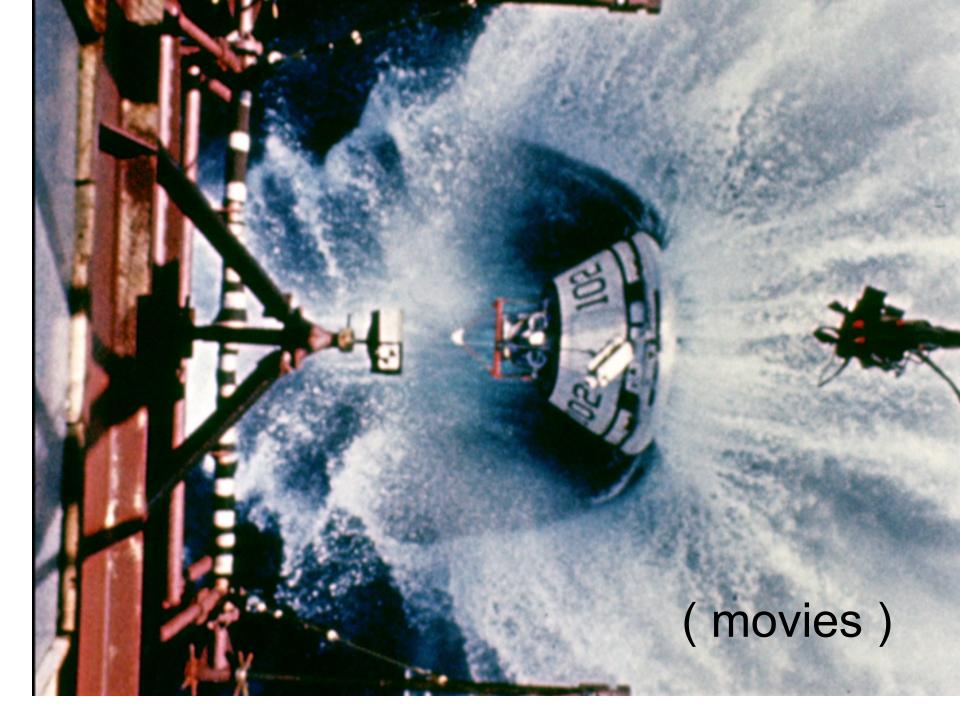
(a) Nominal uprighting (three-bag) in the tank.



Full-scale splashdown tests at North American Aviation







DYNAMIC MODEL INVESTIGATION OF WATER PRESSURES AND ACCELERATIONS ENCOUNTERED DURING LANDINGS OF THE APOLLO SPACECRAFT



NASA TN D-3980

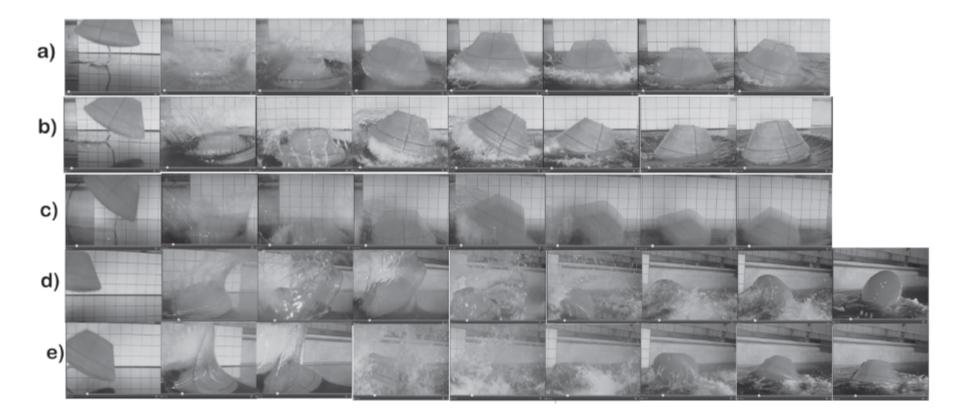
C.1

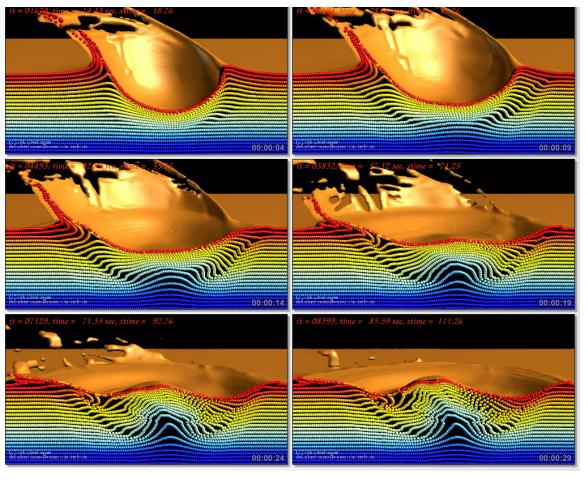
by Sandy M. Stubbs

Langley Research Center

Langley Station, Hampton, Va.



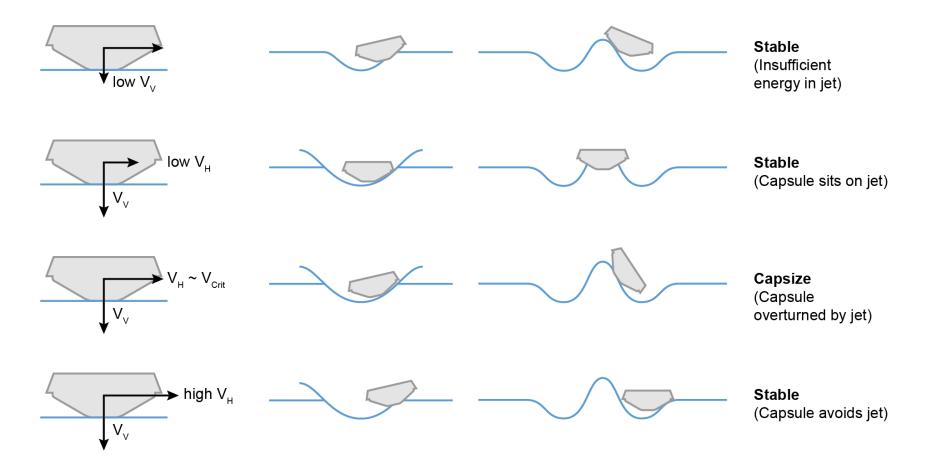




Resurge is well-known in impact cratering as the mechanism for central peak formation.

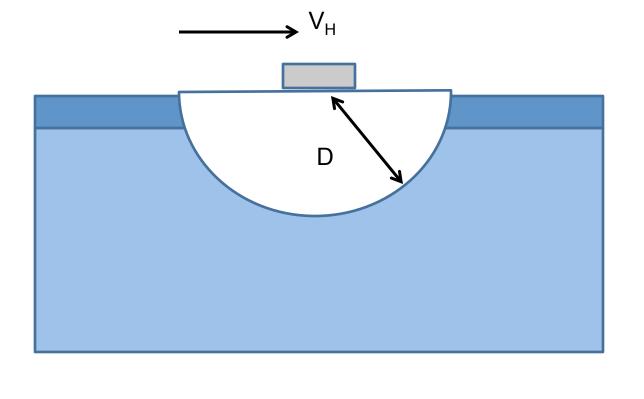






2 necessary conditions for capsize :

- resurging jet must have enough energy to overturn capsule
- jet timing must be right, to catch edge of capsule

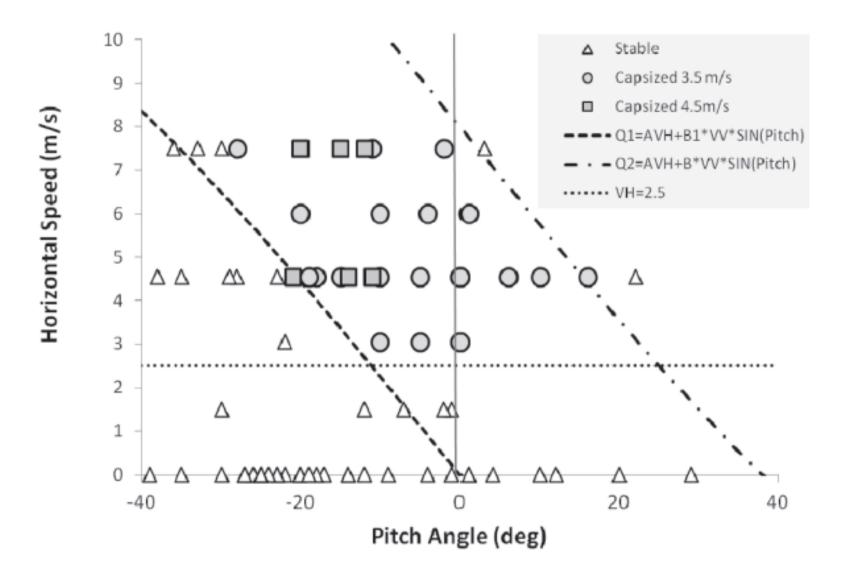


Resurge timescale $t= 2(D/g)^{0.5}$

If average V_H applies, then critical velocity is $V_H \sim L/2t$

In reality some correction factor applies, since resurge is not impulsive, and horizontal velocity of vehicle changes throughout event. To fit a threshold speed V_t for full-scale Apollo of 5m/s we obtain

 $V_t{\sim}0.65 Lg^{5/8}\rho^{1/8}\,m^{\text{-}1/8}\,V_v^{\text{-}1/4}$



Applying the formula $V_t \sim 0.65 Lg^{5/8} \rho^{1/8} \, m^{-1/8} \, V_v^{-1/4}$ to ½ scale Apollo, we find a threshold speed of 2.65 m/s, which agrees nicely with Stubbs' results. This formula can be applied to other vehicles, and other planets/liquids.

Conclusions

Attention in splashdown has traditionally focussed on the first milliseconds after contact. This is an analytically appealing problem with a rich pedigree, and is when the peak deceleration is generated.

The late stages are computationally-demanding and complex. They are, however, critical in the stability of the vehicle.

While complex, the phenomena are deterministic. A simple physical mechanism has been proposed, with a critical horizontal velocity range which defines where capsize may occur. This mechanism, curiously, does not appear to have been discussed in the literature to date.

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