

PHOEBUS a hypervelocity entry demonstrator

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Introducing PHOEBUS Project for a High-speed Of Entry Ballistic multi-User System

- Technological objectives
- Rationale
- Relevance
- Heritage

An aerothermodynamics assessment

- A parametric analysis of the re-entry phase
- A non-equilibrium reacting CFD analysis...
- ...with radiation transport

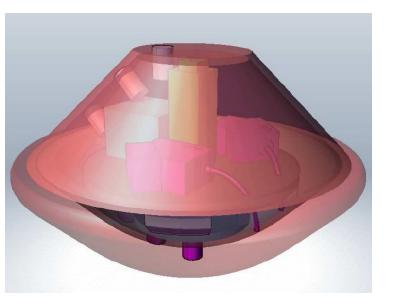
Final remarks

Technological Objectives



First ESA Demonstrator for high speed entry applications

- Maturation and demonstration of critical technologies for:
 - ✓ Materials for Thermal Protection Systems (light ablators)
 - ✓ Aerothermodynamics Tools (uncertainties)
 - ✓ Entry Descent and Landing Systems
 - ✓ Concepts for crushable structures
 - ✓ Sensors for harsh environments
 - ✓ Data for design for demise
 - ✓ Data for space surveillance
 - ✓ Data for civil security
 - ✓ Radiation Data Base
 - ✓ Recovery operations...



Rationale



		E cono LAV	PHOEBUS
Objective	Flight platform for data acquisition on critical LEO-entry aerothermodynamics	Intermediate system demonstrator for LEO operations	Technologies demonstrator for hypervelocity entries
Beneficial for	Aerothermodynamics design of mission to LEO	Cargo and Human Space Transportation from/to LEO	Small sample return missions from Moon, Mars, NEO, Lagrange Points
Entry speed	5 km/s (sub-orbital)	7 km/s (orbital)	12 km/s (hyperbolic)
TPS	Metallic & ceramic	Ceramic & ablator	Lightweight ablator
EDL	Ballistic & supersonic parachute	Aerodynamic controlled & supersonic parachute	Ballistic & crushable structure



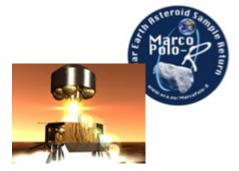
Useful for Science, Robotic Exploration and Human Space Flight Missions

- ✓ Pathfinder for any sample return mission
- ✓ Mastering technologies for hard landing
- ✓ Mastering sensors for harsh environments

Crosslink contribution to

- ✓ CleanSpace Program, Design for Demise
- Surveillance of space (hypervelocity impact)
- ✓ Civil security (hypervelocity entry)

SME's role improvement (better positioning in the market)

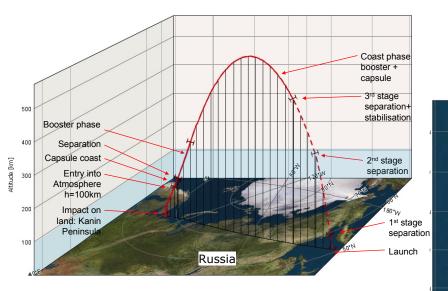




Heritage

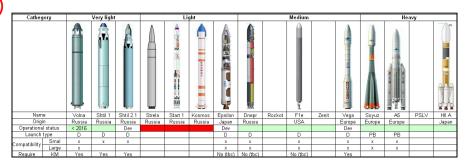


- Preliminary cooperation with KAIST
- 2 GSP (2008-2009) industrial phase A studies (TAS and AST primes, support from Makeev SRC)
- Different solutions found (but feasibility with Volna established)
- □ CDF study in Feb. 2011
- Four years development plan (Phase B/D) beginning of Phase B planned in 2012



A typical trajectory (left) and landing dispersion (right) : Volna case

- The Concurrent Design Facility (CDF) at ESA-ESTEC is an integrated design environment for interdisciplinary and inter-directorate applications, based on concurrent engineering methodology
 - Real-time interaction between disciplines
 - Complete sharing of system/subsystem data
 - Active participation of the customer
 - Teamwork and real-time decision-making



Different launcher considered

Target Spacecraft Mass at Launch 25.00 kg Below Mass Target by Without Margin Margin Total % of Total Dry mass contributions % kg kg Structure 2.35 kg 19.05 0.45 2.79 15.23 Thermal Control 6.10 kg 20.00 1.22 7.32 39.85 Mechanisms 0.00 ka Communications 1.20 kg 20.00 0.24 1.44 7.84 Data Handling 0.92 kg 9.89 0.09 1.01 5.51 GNC 0.28 ka 5.00 0.01 0.29 1.57 Propulsion 0.00 kg 1.80 Power 0.28 ka 20.00 0.06 0.33 Harness 1.00 kg 0.00 0.00 1.00 5.45 Instruments 3.63 kg 15.04 0.55 4.18 22.75 0.00 kg 0.00 0.00 0.00 0.00 Total Dry(excl.adapter) 18.36 kg 15.74 kg System margin (excl.adapter) 20.00 % 3.67 kg Total Dry with margin (excl.adapter) 22.03 kg

ERC mass break down

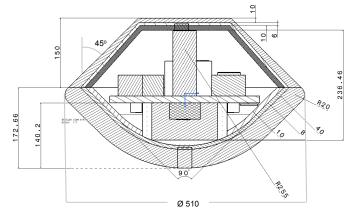
IPPW-9, 16-22 June 2012, Toulouse

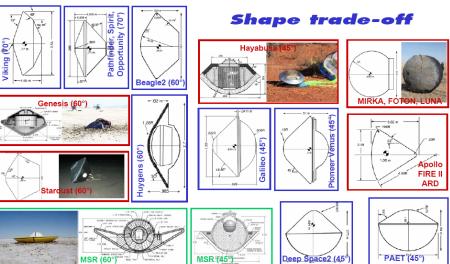
Main technical data

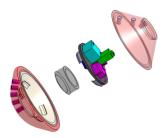
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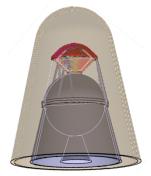
Small, simple capsule (\emptyset = 510 mm, m = 25 kg) to fit in many launchers, (integrated with a solid booster to provide ΔV), costs reduced to the minimum, instrumented:

- Passive descent system, no parachute
- □ Crash resisting memory and beacon
- Data storage for
 - Trajectory, stability & camera data
 - Temperature and pressure on TPS
 - radiative heat flux
- □Passive navigation system, no ACS
- □ (HS-Camera for capturing booster-entry)









Parametric analysis of the re-entry phase



Assumptions

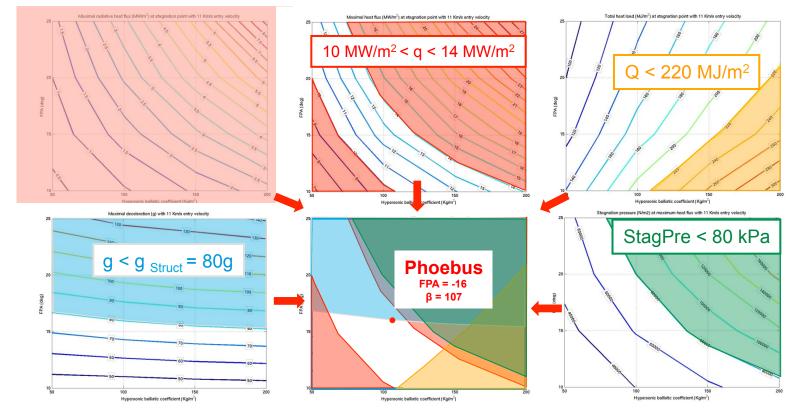
Hayabusa aerodynamics coefficients have been assumed (scaled dimension)
3 degree of freedom TRAJ3D code (FGE)
US 1976 standard model
Detra-Hidalgo (V < 9 km/s) and Tauber-Sutton (9 km/s < V < 16 km/s) formulation for radiative heat flux; Detra and Hidalgo for the convective contribution

Parameters

- entry (inertial) velocity at the interface altitude of 120 km : 8 km/s - 12 km/s
- Flight path angles (FPA): -10 deg to -25 deg
- Different design configurations of the entry capsule have been included considering different ballistic: 50 kg/m² to 200 kg/m²

Constraints / Design Drivers

•(total) maximal heat fluxes below 14 MW/ m² (requirement of DEAM) •to be representative, minimum heat flux (at stagnation point) of 10 MW/m² •total heat load below 220 MJ/m² •maximal deceleration below 80 g •stagnation pressure below 800 mbar at maximum heat flux (14 MW/m²)



A non-equilibrium reacting CFD analysis...



4 points along the trajectory

- Max convective
- **Max radiative**
- Low pressure

High pressure

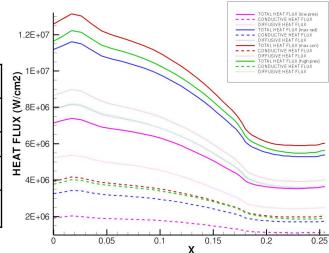
11 species air

2 temperature

- 2 wall conditions:
- **Fully-catalytic**
- non-catalytic

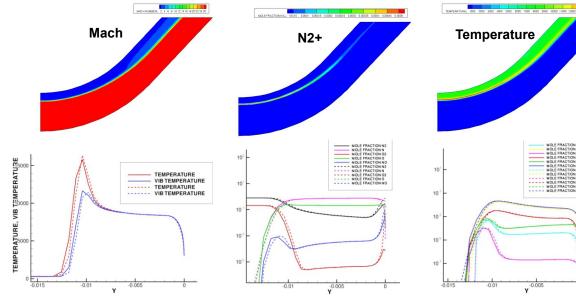
jectory									
	time (s)	altitude (m)	density (kg/m3)	temperature (K)	pressure (Pa)	velocity (m/s)	mach		
test 1: low pressure	18.4	64981	1.64E-04	233.3	10.96	10916	35.65		
test 2: max rad	21.8	55449	5.38E-04	259.5	40.1	10348	32.04		
test 3: max conv	24.1	49464	1.10E-03	270.6	85.28	9518	28.86		
test 4: high pressure	26	45004	2.00E-03	264.2	149.1	8456	25.95		

CFD test matrix

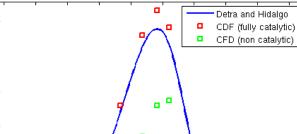


convective (total, conductive and diffusive) heat flux (fc)

Detra and Hidalgo correlation vs CFD computations



Typical 2D plot (top) and stagnation line quantities (bottom) of max convective point (fc, nc)

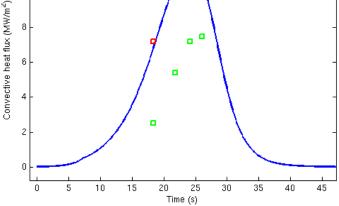


12

10

8

6



Comparison of the simplified correlation and the CFD computations

...with radiation transport

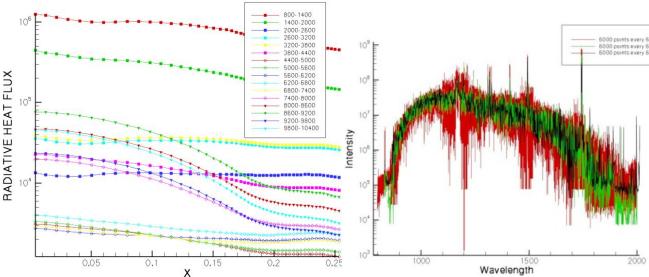


Radiative heat flux on the front (and back) shield computed has been computet (PARADE coupled with a Monte Carlo approach, HERTA)

N, O, N⁺ and O⁺, N₂, O₂, NO, the molecular band systems, N₂ 1st Pos, N₂ 2nd Pos, N₂ Birge-Hopfield, O₂ Schumann-Runge, NO β , NO γ , NO δ , NO ϵ , N₂⁺ 1st Neg and N₂⁺

Equally wavelength discretization in the range between 800 Å and 10400 Å with resolution of 1 Å (for all four points)

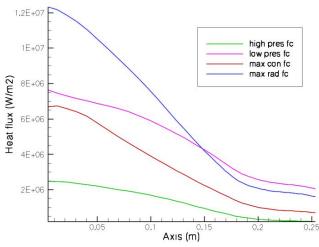
Employing 6000 (adaptive) points for each 600 Å wavelength interval (and 6000 points for each 60 Å wavelength interval) for max radiation point



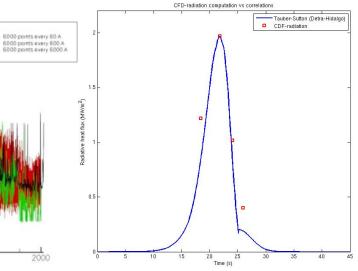
Comparison of the absorption coefficients (VUV range,

stagnation point) calculated with different resolution

Contribution (at stagnation point) of different wavelength (6000 points for each 600 Å wavelength interval)



Radiative heat flux (fc) for the four different trajectory points between 800 Å and 10400 Å with 1 Å resolution



Comparison of the simplified correlation and the CFD-radiation computations

Final remarks: Phoebus is...

... relevant for

✓ Science and Robotic Exploration ✓ Human Space Flight Missions ✓ CleanSpace Program ...

... a challenge mission with respect to ...

 \checkmark EDL strategy \checkmark crushable-structure application (recovery) ✓instrumentation

... which requires more attention on

✓ capsule stability

✓ TPS performance (radiation/ablation, material regression)

... but FEASIBLE











